

Introduction of a Tolerance Factor for the Nd_2CuO_4 (T')-Type Structure

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Received April 22, 1996; accepted May 3, 1996

A tolerance factor, $tf = [3\sqrt{2}r_O + 2\sqrt{6}(r_A + r_O)]/9(r_B + r_O)$, has been established for the Nd_2CuO_4 -type structure, where r_A , r_B , and r_O are the radii of the A , B , and O ions, respectively. It is based on the geometrical matching between the A - O , B - O , and O - O bond distances, and it can be used to distinguish between Nd_2CuO_4 (T')-, T^* -, and K_2NiF_4 (T)-type phases. Using Shannon's ionic radii, it is found that the T' phases occur for $tf < 1.00$ while T phases form for $tf > 1.00$. As expected, the T^* structure exists in a very narrow region between the stability boundaries of these two structure types. The fact that T' and T separate at $tf = 1.00$ suggests that the new tolerance factor model is applicable to both structure types. © 1996 Academic Press, Inc.

INTRODUCTION

The discovery of the superconductivity in the T -type (La , Ba) $_2\text{CuO}_4$ and T' -type (Nd , Ce) $_2\text{CuO}_4$ has motivated study of crystal chemistry and physical properties of the cuprates having these structures (1, 2). The T (K_2NiF_4) structure of the ternary oxides $A_2\text{BO}_4$ can be described as an intergrowth of ABO_3 perovskite- and AO rock-salt layers along the c -axis, containing corner-shared BO_6 octahedra and AO_9 polyhedra. In contrast, the T' (Nd_2CuO_4) structure is derived from an intergrowth of BO_2 infinite layer sheets and A_2O_2 fluorite-type layers along the c -axis, containing corner-shared BO_4 square planes and AO_8 cubes. Although the cation arrangements in both the T' - and T -type structures are the same, their anion configurations are different. The T^* structure consists of a hybrid of the T and T' structures (3). The structure of the T' -type Nd_2CuO_4 is presented in Fig. 1.

Several research groups recently have investigated the stability of the T and T' structural types using the well-known Goldschmidt tolerance factor t as a criterion. This tolerance factor (also called the perovskite tolerance factor) is based on an analysis of the perovskite subcell of the structure and is defined as

$$t = (r_A + r_O)/\sqrt{2}(r_B + r_O), \quad [1]$$

where r_A , r_B , and r_O are the radii of the A , B , and O ions, respectively (4–8). It was found that phases with the T -type structure fall in the range $0.87 < t < 0.99$ while those with the T' -type exist for $0.83 < t < 0.86$ (5). If the phases Ln_2CuO_4 ($\text{Ln} = \text{Dy}$, Ho , Er , Tm , Y), prepared under high pressure (9), are included, the lower limit of t for the T' phases extends to 0.81. The T^* phases occur at tolerance factors between t of the T and T' phases.

The Goldschmidt tolerance factor provides an excellent guide for predicting when perovskite-related structures may be expected, and for classifying the structural type of compounds with the general formula ABX_3 , and it has been in use for over half a century. The tolerance factor is based on the geometrical matching between the A - X and B - X layers in the cubic perovskite structure. However, the A atom is in twelve-coordination for the perovskite structure but in nine-coordination for the T -type structure. In fact, the A - O bond in the T -type structure exhibits features of both the twelve-coordination of perovskite and the six-coordination of rock salt. Perhaps for these reasons, most t values for the T phases are closer to the lower t limit (4, 5). In addition, the structure of the T^* -type $\text{CaSmCuO}_3\text{Cl}$ has been determined by single crystal X-ray diffraction (10). Unfortunately, its t value (0.842) is near the center of the T' field. In order to address these issues, we introduce a Nd_2CuO_4 -type tolerance factor tf , based on the geometrical matching between the A - O , B - O , and O - O distances.

MODEL OF THE T' -TYPE TOLERANCE FACTOR tf

We assume that the AO_8 cube has an idea CsCl -type structure in the T' phase and that all ions are spherical with rigid contact to each other. The edge length L_c of the cube can be expressed as

$$L_c = a_{A-O}/\sqrt{2} \quad [2]$$

and

$$L_c = 2(r_A + r_O)/\sqrt{3}. \quad [3]$$

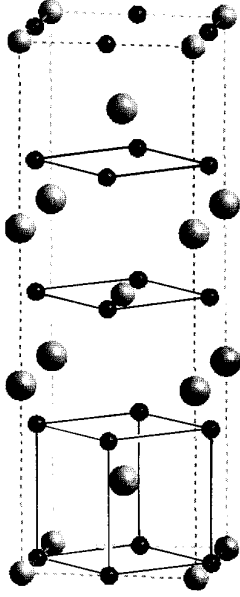


FIG. 1. Structure of the T' -type Nd_2CuO_4 . Large, medium, and small balls represent Nd, Cu, and O atoms, respectively.

Substituting Eq. [2] into [3], the relationship between the a lattice parameter and the bond distances can be written as

$$a_{A-O} = 2\sqrt{6}(r_A + r_O)/3. \quad [4]$$

In addition,

$$a_{B-O} = 2(r_B + r_O) \quad [5]$$

and

$$a_{O-O} = \sqrt{2}(r_O + r_O) = 2\sqrt{2}r_O, \quad [6]$$

where a_{A-O} , a_{B-O} , and a_{O-O} are the a lattice parameters for equilibrium $A-O$, $B-O$, and $O-O$ bond distances, respectively. r_A is the radius of the eight-coordinated cation, r_B is radius of the square-planar-coordinated cation, and r_O is the radius of the six-coordinated oxygen ion.

From Shannon's ionic radii (11), the a lattice parameter $a_{A-O} = 2\sqrt{6}(r_A + r_O)/3$ for the T' -type Nd_2CuO_4 is 10.7% greater than $a(T)_{A-O} = \sqrt{2}(r_A + r_O)$ for the T -type La_2CuO_4 , where $a(T)_{A-O}$ is the a parameter based upon the $A-O$ distance for the T -type structure and r_A is the radius of the nine-coordinated La^{+3} . The real difference between a of Nd_2CuO_4 and a of La_2CuO_4 is only 3.6% (12). The geometrical matching can be reached by expanding the $B-O$ layers and elongating the AO_8 cubes along the c -axis. As a result, the $O-O$ distance is only 279 pm in the (004) planes but 304 pm along the c -axis for Nd_2CuO_4 . As the size of A decreases, the electrostatic repulsion between

the coplanar oxygens in the fluorite layers increases. Based on the consideration of the competition between the $A-O$ attraction and $O-O$ repulsion, as well as the geometrical matching between the bond distances, a tolerance factor tf for the Nd_2CuO_4 (T')-type structure is proposed as

$$tf = [1/3 a_{O-O} + 2/3 a_{A-O}]/a_{B-O}. \quad [7]$$

The weighting of factors in the numerator reflects the fact that the number of $A-O$ bonds is twice the number of the $O-O$ bonds in the (004) planes in the unit cell. Substituting Eqs. [4], [5], and [6] into [7], tf can be expressed as

$$tf = [3\sqrt{2}r_O + 2\sqrt{6}(r_A + r_O)]/9(r_B + r_O) \quad [8]$$

or

$$tf = [(3\sqrt{2} + 2\sqrt{6})r_O + 2\sqrt{6}r_A]/9(r_B + r_O). \quad [9]$$

TEST OF THE TOLERANCE FACTOR tf

The T' tolerance factor tf values for the T' -, T^* -, and T -type $A_2\text{BO}_4$ were calculated by employing Shannon's ionic radii (11). The $A_2\text{BO}_4$ phases, studied by Bringley *et al.* for their stability limits using the perovskite-type tolerance factor t (5), were selected for the test of tf . However, the T phases, for which the r_B values are not available in Ref. (11), were not included. Since these phases have the t values between 0.915 and 0.976, excluding them would not affect the determination of the stability limit of the T phases. $\text{La}_{1.5}\text{Nd}_{0.5}\text{CuO}_4$ was also rejected because the T' phase at this composition has been reported to be thermodynamically different from the T' phase at lower La concentration (6, 7). The T' -type Ln_2CuO_4 ($\text{Ln} = \text{Dy}, \text{Ho}, \text{Er}, \text{Tm}, \text{Y}$) and La_2PdO_4 and the T -type Ca_2GeO_4 and Sr_2VO_4 were included in the analysis (9, 13–15). The latter two adopt more than one structural type (16).

Since the four-coordinated radius of V^{+4} is not available in Ref. (11), the average $\text{V}^{+4}-\text{O}$ bond distance (180.5 pm) of the K_2SO_4 -type S_2VO_4 was taken (16). For the same reason, the $\text{Cu}^{+3}-\text{O}$ bond distance (183 pm) found in the NaCuO_2 phase was used for LaSrCuO_4 (17). Comparison of the tolerance factors tf and t for $A_2\text{BO}_4$ are summarized in Table 1.

RESULTS AND DISCUSSION

This study shows that the T' phases exhibit tolerance factors in the range $1.00 > tf > 0.96$ while the T phases occur for $1.00 < tf < 1.14$. The T^* phases, as expected, exist in a very narrow region between the T and T' boundaries. A high temperature phase transition from the K_2SO_4 - to T -type was found in Sr_2VO_4 (15, 16). Its $tf = 1.131$ value is near the high limit of the T phases, suggesting the region

TABLE 1
Comparison of the Tolerance Factors *tf* and *t* for the A₂BO₄ Compounds

A ₂	B	<i>tf</i>	<i>t</i>	A ₂	B	<i>tf</i>	<i>t</i>
<i>T</i> -type (A ₂ BO ₄)							
Sr ₂	Mn	1.141	0.993	Sr ₂	V	1.131	0.968 ^b
LaSr	Al	1.126	0.973	Sr ₂	Ti	1.122	0.956
LaSr	Cu	1.101	0.971	Ca ₂	Mn	1.098	0.945
Ca ₂	Ge	1.098	0.945 ^a	LaSr	Ga	1.077	0.932
PrSr	Fe	1.061	0.914	GdSr	Fe	1.051	0.902
Sr ₂	Sn	1.047	0.917	Ba ₂	Pb	1.039	0.933
La ₂	Ni	1.019	0.885	La _{1.9} Sr _{0.1}	Cu	1.014	0.879
Pr ₂	Ni	1.010	0.873 ^c	La ₂	Cu	1.009	0.868 ^c
Nd ₂	Ni	1.005	0.867 ^c	La ₂	Co	1.004	0.865 ^c
<i>T'</i> -type (A ₂ BO ₄)							
Pr ₂	Cu	0.999	0.856	Nd ₂	Cu	0.995	0.851
Nd _{1.85} Ce _{0.15}	Cu	0.991	0.847	Sm ₂	Cu	0.986	0.841
Eu ₂	Cu	0.983	0.837	Gd ₂	Cu	0.979	0.832
La ₂	Pd	0.974	0.818	Dy ₂	Cu	0.972	0.824 ^a
Y ₂	Cu	0.970	0.822 ^a	Ho ₂	Cu	0.969	0.821 ^a
Er ₂	Cu	0.966	0.817 ^a	Tm ₂	Cu	0.963	0.814 ^a
A ₂		<i>tf</i>	<i>t</i>	A ₂		<i>tf</i>	<i>t</i>
<i>T*</i> -type (A ₂ CuO ₄)							
La _{0.85} Eu _{0.9} Sr _{0.25}		1.001	0.859	LaGd _{0.8} Sr _{0.2}		1.000	0.857
La _{0.8} SmSr _{0.2}		1.000	0.858	La _{0.75} SmSr _{0.25}		1.000	0.858
La _{0.82} SmSr _{0.18}		1.000	0.857	La _{1.1} Eu _{0.8} Sr _{0.1}		1.000	0.857
La _{0.9} Eu _{0.9} Sr _{0.2}		1.000	0.857	La _{0.8} EuSr _{0.2}		0.999	0.856
La _{1.3} Tb _{0.7}		0.999	0.855	La _{1.4} Tb _{0.6}		0.999	0.856
La _{0.9} Y _{0.8} Sr _{0.3}		0.997	0.855	LaDy _{0.8} Sr _{0.2}		0.997	0.854
LaEu _{0.9} Sr _{0.1}		0.997	0.855	La _{1.2} Dy _{0.8}		0.994	0.851

^a High pressure form.

^b High temperature form.

^c Orthorhombic.

with *tf* greater than this value could belong to the K₂SO₄-type field, except that of (1.141) for Sr₂MnO₄. The result of the computation of the *tf* values for the K₂SO₄-type phases Ca₂SiO₄, Sr₂MO₄ (*M* = Si, Ge), and Ba₂MO₄ (*M* = Ti, Ge, V) confirms the expectation (18).

Besides temperature, pressure also greatly affects the stability limit of the *T'* and *T* phases. For example, a high pressure phase transition from olivine-type, having six-coordinated *A* and four-coordinated *B*, to *T*-type was found in Ca₂GeO₄ (14). In addition, the *T'* phases Ln₂CuO₄ (*Ln* = Dy, Ho, Er, Tm, Y) with *tf* ≤ 0.972 can only be prepared at high pressure due to the presence of the small size of *Ln* (9). Both examples follow a general rule that the coordination number of the cation increases with pressure.

The *tf* value for the *T**-type CaSmCuO₃Cl is 0.993 (10). The result is better than that of *t* = 0.842 calculated by the perovskite tolerance factor as mentioned earlier. The tolerance factor *tf* also can be applied to the *T*-type halides and sulfides (19, 20). For example, the *tf* values for K₂NiF₄

(1.121), K₂CuF₄ (1.109), Ba₂HfS₄ (1.064), and Ba₂ZrS₄ (1.060) all fall in the predicted field.

CONCLUSIONS

A new tolerance factor *tf* for the Nd₂CuO₄-type structure has been proposed based on the geometrical matching between the *A*-O, *B*-O, and O-O bond distances. It has been successfully applied in the investigation of the structural stability of the *T'*, *T*, and *T** phases. Surprisingly, the *T* and *T'* phases are perfectly separated by an "ideal" tolerance factor *tf* = 1.00, suggesting that the model relates accurately to the ionic packing factors of the *T'* and *T* structures, and clearly showing that *tf* is a very powerful classification parameter.

ACKNOWLEDGMENT

The author thanks Dr. Bruce W. Scott and Professor David Walker for very helpful discussions. This work is contribution number 5526 from

the Lamont-Doherty Earth Observatory of Columbia University and was supported by the National Science Foundation and the Department of Energy.

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